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| (21) International Application Number: PCT/AU93/00281 (22) International Filing Date: 16 June 1993 (16.06.93) (30) Priority data: PL 2991 16 June 1992 (16.06.92) AU (71) Applicant (for all designated States except US): COMMON-WEALTH SCIENTIFIC AND INDUSTRIAL RESEARCH ORGANISATION [AU/AU]; Limestone Avenue, Campbell, ACT 2601 (AU). (72) Inventors; and (75) Inventors/Applicants (for US only) : ANDERSON, Nevil, James [AU/AU]; 3 Victory Street, Sandringham, VIC 3191 (AU). KOLARIK, Luis, Otakar [AU/AU]; 21 Rowitta Drive, Glen Waverley, VIC 3150 (AU). | | (74) Agents: CORBETT, Terence, Guy et al.; Davies Collison Cave, 1 Little Collins Street, Melbourne, VIC 3000 (AU). (81) Designated States: AU, BB, BG, BR, BY, CA, CZ, FI, HU, JP, KP, KR, KZ, LK, MG, MN, MW, NO, NZ, PL, RO, RU, SD, SK, UA, US, VN, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, ML, MR, NE, SN, TD, TG). Published <i>With international search report.</i> |
| (54) Title: PROCESS FOR RECOVERING INORGANIC COAGULANTS FROM WATER OR WASTE WATER TREATMENT SLUDGES (57) Abstract The invention is concerned with the recovery of inorganic coagulants used in water or waste water treatment processes from the coagulant-containing sludges produced in such processes. The method consists of the following steps: 1) treatment of the sludge with acidic or alkaline material as appropriate in order to dissolve the coagulant; 2) adjustment of liquor pH to 2 - 3, if necessary; 3) addition of polyelectrolyte and optionally a solid adsorbent to the liquor to cause precipitation of some impurities; 4) separation of the liquor containing dissolved coagulant from the residue; 5) contact of the supernatant from step 4 with a positively charged and/or hydrophobic solid adsorbent to remove soluble organic materials. The process described has the dual benefit of reducing the volume of sludge for disposal, and reducing the amount of fresh coagulant needed and hence saving on coagulant costs. | | |

Process for recovering inorganic coagulants from water or waste water treatment sludges.

This invention is concerned with the recovery for recycling of inorganic coagulants used
5 in water or waste water treatment processes from the coagulant-containing sludges
produced in such processes. The process described has the dual benefit of reducing the
volume of sludge for disposal, and reducing the amount of fresh coagulant needed and
hence saving on coagulant costs.

10 Bibliographic details of the publications referred to in this specification are collected at
the end of the description.

In order to satisfy the ever increasing thirst of our industrialised and urbanised societies,
water authorities must turn to treatment of more and more polluted water sources using
15 complex technologies. This creates a secondary problem - the disposal of
residues/sludges formed as a result of the treatment. Usually such residues contain
substantial quantities of inorganic coagulant such as aluminium or ferric hydroxides
which create much bulk and make the sludge less than beneficial to the environment into
which it is discharged.

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Coagulants are used to encourage the agglomeration of colloidal impurities in many
water/wastewater purification processes; commonly the agglomerated impurities are then
removed from the product water by sedimentation or filtration. The coagulants may be
either organic or inorganic in nature. The inorganic coagulants are usually based on iron
25 or aluminium, most commonly used are aluminium sulphate (alum) or ferric sulphate or
chloride.

Past attempts to recover and reuse alum in conventional water treatment processes were
usually motivated by problems associated with the handling and disposal of the
30 aluminium hydroxide containing sludges. Recovery of alum reduces the amount of solids
and improves the dewatering and filtration characteristics of the residue. Reuse of the
recovered alum also reduces the chemical cost.

alkali there are a number of problems to overcome. Firstly, the amount of acid or alkali required is affected by both the amount of water present and the age of the sludge. Because the cheap dewatering processes are slow the sludge ages during the process. Secondly, during redissolution, organic acids and heavy metals are liberated if present in the residue. Aged sludge requires lower pH for redissolution of the polymerised aluminium hydroxide which also increases the concentration of other undesirable components in the recovered stream. In the present state of the art only approximately 50-70% of the recovered coagulant can be reused safely.

10 To improve the aluminium recovery rate and to enhance its separation from impurities, techniques such as liquid ion exchange ⁽¹¹⁾, electrochemical coagulant regeneration ⁽¹²⁾, ultrafiltration ⁽¹³⁾, and selective two-step aluminium recovery employing composite membrane ⁽¹⁴⁾, have been evaluated in the laboratory. It remains to be seen whether such techniques are economic in a practical situation.

15

Thus there is a need for a simple technique which would allow recovery of the inorganic coagulant selectively, leaving the unwanted impurities, such as humic and fulvic acids, behind. We have discovered a relatively simple separation process that meets this need and which may be incorporated into water treatment plants that use inorganic coagulants.

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Accordingly this invention provides a method for recovering inorganic coagulants from water/wastewater treatment sludges in a condition which enables effective reuse of the coagulant, which method comprises the following steps:

1. Treatment of the sludge with acidic or alkaline material as appropriate in order to dissolve the coagulant.
2. Precipitation of humic acids by adjustment of liquor pH (usually to 2 - 3).
3. Addition of polyelectrolyte and optionally a solid adsorbent to the liquor to cause precipitation of impurities.
4. Separation of the liquor containing dissolved coagulant from the residue.
- 30 5. Contact of the supernatant from step 4 with a positively charged and/or hydrophobic solid adsorbent to remove soluble organic materials.

Accordingly, in another aspect, this invention provides a process for recovery of inorganic coagulant from water treatment sludges which comprises steps 1 - 5 above, followed by (as and when necessary) subjecting the impurity coated positively-charged PC/H Adsorbent to a physical process thereby to remove the coating of impurities from the
5: PC/H Adsorbent, separating the removed impurities from the PC/H Adsorbent and returning the cleaned PC/H Adsorbent to the process.

The process of the invention is further described in the following non-limiting examples.

10 **EXAMPLE 1**

A water treatment sludge was treated at pH 2.5 using dilute sulphuric acid. The liquor was then separated from the sludge and treated with polyelectrolyte to precipitate a second sludge. The supernatant from polyelectrolyte treatment was an aluminium rich solution with an initial colour of 460 PCU and a Total Organic Carbon (TOC) content
15 of 190 mg/L. This solution was passed through columns of Amberlite IRA 910 in either the hydroxyl or sulphate form. The hydroxyl column eluent had an average colour of 100 PCU and TOC 40mg/L; the sulphate column eluent had an average colour of 120 PCU and 50mg/L TOC.

Each column passed all of the aluminium initially present.

20 When the impurity coated resins were washed with water, the hydroxyl column released impurities equivalent to 55% of the initial colour and 42% of the TOC while the sulphate column released 28% of the colour and 24% of the TOC. Further treatment of each column with 0.5M NaOH released impurities equivalent to 45% of the initial colour and 58% of the initial TOC from the hydroxyl column and 72% of the initial colour and 58%
25 of the initial TOC from the sulphate column.

EXAMPLE 2

A sludge from the SIROFLOC[®] process was treated with acid at pH 2.5, a cationic polyelectrolyte was added to the supernatant from the acid treatment. A flocculant
30 precipitate formed which was allowed to settle. The supernatant from the polyelectrolyte treatment had pH 2.95, an aluminium content of 317 mg/L, apparent colour = 1080 PCU, and TOC = 164 mg/L.

Table 5. Adsorption of humic substances from acidic regeneration effluent by ion exchange resins.

Table 5. Adsorption of nitrate anions from waste regeneration effluent.

| Type | Source | Code | Flow Rate BV/hr | Length of Run BV | Average Removal | | Recovered by Regen. % | | Efficiency Recovered Al % |
|---|-------------|--------------------------|--------------------|------------------------|--------------------|-----|--------------------------|-----|---------------------------------|
| | | | | | TOC | Col | TOC | Col | |
| Untreated regeneration effluent | | | | | | | | | |
| Monofunctional C ₁₈ sorbent | Millipore | C ₁₈ SepPak | 12 | 70 | | 49 | ND | ND | ND |
| Trifunctional bonded C ₁₈ sorbent | Millipore | 1 C ₁₈ SepPak | 20 | 80 | 76 | 82 | ND | 72 | 95 |
| Styrene polymeric adsorbent | Rohm & Haas | 1.1 ml bed XAD 2 | 20 | 70 | 50 | 49 | ND | 48 | 88 |
| " | " | XAD 4 | 20 | 70 | 54 | 53 | ND | 38 | ND |
| " | " | XAD 7 | 20 | 70 | 58 | 59 | ND | 36 | ND |
| Acrylic polymeric adsorbent | " | XAD 8 | 20 | 70 | 54 | 52 | ND | 40 | ND |
| Acrylic gel Type I | " | 5 ml IRA 958 | 8.6 | 145 | 57 | 68 | 96 | 101 | 92 |
| Styrene macroreticular Type II | " | 5 ml IRA 910 | 8.6 | 115 | 54 | 59 | 98 | 88 | 92 |
| Styrene DVB Macroreticular | " | 5 ml IRA 904 | 8.6 | 100 | 60 | 59 | 117 | 104 | ND |
| Activated carbon | Hydradarco | | 6 | 30 | 85 | 92 | 84 | 45 | 82 |
| Silica gel | | | 20 | 70 | 44 | 39 | ND | 56 | ND |
| Cotton Wool | | | 20 | 70 | ND | 39 | ND | 40 | ND |
| Cellulose | | | 6 | 70 | ND | 56 | ND | 16 | ND |

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CLAIMS

1. A method for recovering inorganic coagulants from water/wastewater treatment
sludges in a condition which enables effective reuse of the coagulant, which method is
5 characterised by the following steps:

- (1) treating the sludge with an acidic or alkaline material, as appropriate, in
order to dissolve the coagulant to produce a liquor containing the dissolved
coagulant from the sludge;
- (2) precipitating humic acids by adjustment of the pH of the liquor;
- 10 (3) adding a polyelectrolyte, and optionally a solid adsorbent, to the liquor to
cause precipitation of impurities;
- (4) separating the liquor containing dissolved coagulant from the residue;
- and
- (5) contacting the supernatant liquor from step (4) with a positively-charged
15 and/or hydrophobic solid adsorbent to remove soluble organic materials.

2. A method as claimed in Claim 1, characterised in that the impurity coated
positively-charged and/or hydrophobic solid adsorbent ("PC/H adsorbent") obtained in
step (5) is subjected to a physical process to remove the coating of impurities from the
20 PC/H adsorbent, the removed impurities are separated from the PC/H adsorbent and the
cleaned PC/H adsorbent is returned to process step (5).

3. A method as claimed in Claim 1 or Claim 2, characterised in that the
polyelectrolyte is an anionic polyelectrolyte.
25

4. A method as claimed in any one of the preceding Claims, characterised in that the
the adsorbent for step (3) is a natural or artificial clay mineral or a particulate carbon.

30 5. A method as claimed in any one of the preceding Claims, characterised in that the
positively charged and/or hydrophobic adsorbent (the "PC/H Adsorbent") used in step (5)

INTERNATIONAL SEARCH REPORT

International application No.

PCT/AU 93/00281

A. CLASSIFICATION OF SUBJECT MATTER

Int. Cl.⁵ C02F 011/00; C02F 011/12

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC C02F 011/00; C02F 011/12; C02B 001/20; C02C 003/00; C02C 005/02.

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched
AU:IPC as above

Electronic data base consulted during the international search (name of data base, and where practicable, search terms used)

DERWENT:IPC as above

search terms: coag: (for C02F 11/00 & 11/12); coag: and humic(s) acid and polyelectrolyte (for C02C 3/00 & 5/02; humic(s) acid and polyelectrolyte (for C02B 1/20). Chemical Abstracts: sludge and (water or H₂O or aque:) and coag: and (humic(s) acid).

C. DOCUMENTS CONSIDERED TO BE RELEVANT

| Category * | Citation of document, with indication, where appropriate, of the relevant passages | Relevant to Claim No. |
|------------|--|-----------------------|
| A | US,A, 3959133 (METCALF & EDDY, INC.) 25 May 1976 (25.05.76) | 1-6 |
| A | US,A, 3901804 (KANZAKI PAPER MANUFACTURING CO. LTD.) 26 August 1975 (26.08.75). | 1-6 |
| A | Derwent Abstract Accession No. 13587Y/08, Class D15 F09, JP,A, 52-003256 (MITSUBISHI HEAVY IND KK) 11 January 1977 (11.01.77) | 1-6 |

☒ Further documents are listed
in the continuation of Box C.

☒ See patent family annex.

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INTERNATIONAL SEARCH REPORT
Information on patent family members

International application No.
PCT/AU 93/00281

This Annex lists the known "A" publication level patent family members relating to the patent documents cited in the above-mentioned international search report. The Australian Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

| Patent Document Cited in Search Report | | Patent Family Member | | | | | |
|--|---------|----------------------|---------|----|----------|----|--------|
| US | 3901804 | FR | 2208846 | JP | 49065052 | SE | 388412 |
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